

**UNCLASSIFIED**

---

**AD 274 397**

*Reproduced  
by the*

**ARMED SERVICES TECHNICAL INFORMATION AGENCY  
ARLINGTON HALL STATION  
ARLINGTON 12, VIRGINIA**



---

**UNCLASSIFIED**

NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U. S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

CATALOGED BY ASTIA  
AS AD NO. 274397

## COMPUTATION OF VISUAL RANGE IN FOG AND LOW CLOUDS

Don R. Dickson

J. Vern Hales

Scientific Report #3

AF 19(604)-7333

Project No. 8641

Task No. 86411

December 1961

ASTIA

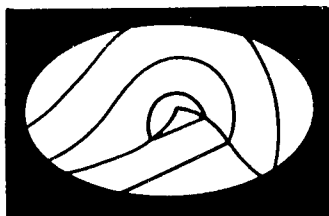
APR 23 1962

62-3 /

Prepared For

GEOPHYSICS RESEARCH DIRECTORATE  
AIR FORCE CAMBRIDGE RESEARCH LABORATORIES  
OFFICE OF AEROSPACE RESEARCH  
UNITED STATES AIR FORCE  
BEDFORD, MASSACHUSETTS

458430



**Intermountain Weather, Inc.**

*Consulting and Research • Weather Forecasting • Instruments*

P.O. BOX 88

SALT LAKE CITY 10, UTAH

DA 2-1178

Requests for additional copies by Agencies of the Department of Defense, their contractors, and other government agencies should be directed to the:

Armed Services Technical Information Agency  
Arlington Hall Station  
Arlington 12, Virginia

Department of Defense contractors must be established for ASTIA services, or have their 'need-to-know' certified by the cognizant military agency of their project or contract.

All other persons and organizations should apply to the:

U.S. DEPARTMENT OF COMMERCE  
OFFICE OF TECHNICAL SERVICES  
WASHINGTON 25, D. C.

# COMPUTATION OF VISUAL RANGE IN FOG AND LOW CLOUDS

Don R. Dickson

J. Vern Hales

Scientific Report #3

AF 19(604)-7333

Project No. 8641

Task No. 86411

December 1961

Prepared For

GEOPHYSICS RESEARCH DIRECTORATE  
AIR FORCE CAMBRIDGE RESEARCH LABORATORIES  
OFFICE OF AEROSPACE RESEARCH  
UNITED STATES AIR FORCE  
BEDFORD, MASSACHUSETTS



**Intermountain Weather, Inc.**

*Consulting and Research • Weather Forecasting • Instruments*

P.O. BOX 88

SALT LAKE CITY 10, UTAH

DA 2-1178

ACKNOWLEDGMENTS

The authors wish to thank Dr. Franklin S. Harris, Jr. and Mr. Donald Henderson for their helpful suggestions.

We are indebted to the Air Force Cambridge Research Laboratories for financial support, and in particular to Dr. Wayne D. Mount and Mr. Iver A. Lund for their personal encouragement, which has been invaluable.

ABSTRACT

Visual ranges were computed for various values of extinction coefficient, for five sets of conditions appropriate to fog and low clouds. The computations involve basic theories of visual range as developed by Allard (1876) and Koschmieder (1924). The four values of the threshold of illumination ( $E_t$ ) which Haig and Morton (1958) determined were used in the Allard theory computations.

## TABLE OF CONTENTS

	PAGE
ACKNOWLEDGMENTS . . . . .	ii
ABSTRACT . . . . .	iii
LIST OF TABLES . . . . .	v
LIST OF FIGURES . . . . .	vi
SECTION	
1. INTRODUCTION . . . . .	1
2. DEVELOPMENT OF EQUATIONS . . . . .	2
3. THRESHOLD OF ILLUMINATION . . . . .	10
4. EXTINCTION COEFFICIENTS . . . . .	12
5. COMPUTATION OF VISUAL RANGE . . . . .	15
6. CONCLUSION . . . . .	20
REFERENCES . . . . .	21



## LIST OF TABLES

TABLE	PAGE
1. Threshold of illumination ( $E_t$ ) (after Haig and Morton) . . . . .	11
2. Cloud drop size distribution, van de Hulst efficiency factor and attenuation coefficient . . . . .	14
3. The minimum distance that 20% of pilots tested by Haig and Morton could see. . . . .	15
4. The minimum distance that 90% of pilots tested by Haig and Morton could see. . . . .	15
5. The visual ranges for conditions of natural light obtained by use of the Koschmieder equation . . . . .	16
6. Visual ranges for daylight conditions comparing Koschmieder and Allard methods . . . . .	16
7. Water density for the four types of clouds studied . . . . .	17
8. The variation of visual range in an aging fog . . . . .	19

## LIST OF FIGURES

FIGURE	PAGE
1. Illustrating the Koschmieder theory. . . . .	3
2. The minimum distance as a function of the attenuation coefficient as seen by 20% of the pilots tested by Haig and Morton. . . . .	8
3. The minimum distance as a function of the attenuation coefficient as seen by 90% of the pilots tested by Haig and Morton. . . . .	9

## 1. INTRODUCTION

A great need exists for better determinations of visual ranges in fog, low clouds, etc. A forward step in the effort to provide better data was made when the transmissometer AN/GMT-10 was developed.

As has been shown by Haig and Morton (1958), the Allard (1876) law proved to be very useful when used with the transmissometer data. However, an extension to the Haig and Morton work was needed for obtaining visual ranges in stratus clouds and fogs. The extension was made by use of the threshold of illumination values ( $E_t$ ) of Haig and Morton along with the van de Hulst (1957) equation for the extinction coefficient (see equation 25). The drop size distributions of Bricard (1943) and Diem (1942, 1948) were used as first order approximations for fog, although these values were obtained for stratus type clouds.

## 2. DEVELOPMENT OF EQUATIONS

Visual range can be determined analytically by use of one of two basic assumptions. The first one which will be discussed here is the Koschmieder (1924) method. This method assumes that the object which is observed reflects scattered light incident upon it. Figure 1 illustrates this method.

### Assumptions

(a) The atmosphere is considered as a turbid medium containing a large number of small particles.

(b) Each element of volume contains a large number of particles, each of small order of magnitude compared to the volume itself.

(c) The scattering action of each particle is independent of the presence of all the others.

(d) Light scattered from an element of volume will be considered as coming from a point source from which the scattered intensity is proportional to the number of particles.

(e) Light rays will be considered rectilinear; that is to say, atmospheric refraction will not be taken into consideration.

(f) A cloudless sky is assumed.

(g) In a horizontal plane near the surface of the earth, the coefficient of attenuation by scattering,  $b$ , is constant.

(h) The curvature of the earth is not considered.

(i) The linear dimensions of the object are small when

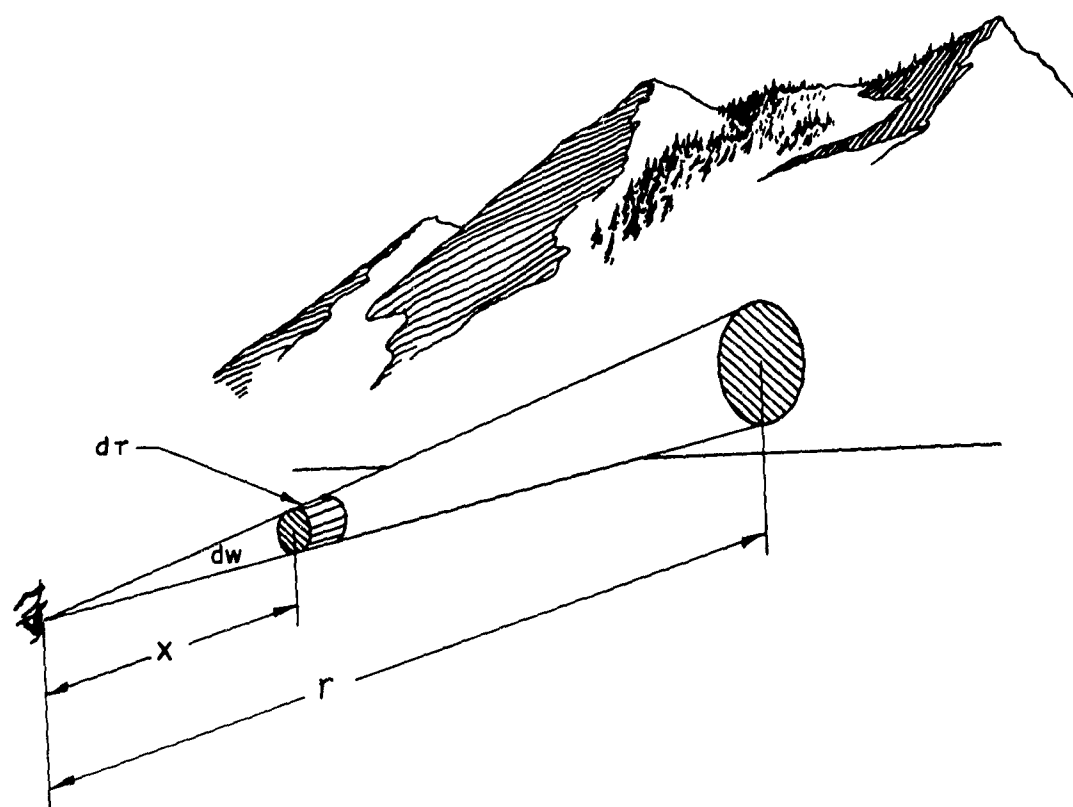


FIG. 1 ILLUSTRATING THE KOSCHMIEDER THEORY

compared to the distance from the observer.

Consider an element of volume

$$d\tau = d\omega x^2 dx, \quad (1)$$

$$dI = d\tau Ab \quad (2)$$

where A is a constant of proportionality to be determined by the boundary conditions and  $b \text{ (cm}^{-1}\text{)}$  is the scattering coefficient.

The illuminance E at the eye due to the light scattered from  $d\tau$  is

$$dE = dI x^{-2} e^{-bx} \quad (3)$$

$$dB = \frac{dE}{d\omega} \quad (4)$$

$$dB = x^{-2} e^{-bx} \frac{dI}{d\omega} . \quad (5)$$

Through use of equations (1) and (2), the following is obtained:

$$dB = Abe^{-bx} dx.$$

We now evaluate A by integration.

Subscript o refers to the apparent luminance of a black object, and subscript h refers to the illuminance of the horizon sky.

$$B_o = \int_0^r Abe^{-bx} dx = A(1 - e^{-br}) \quad (6)$$

$$B_h = \int_0^\infty Abe^{-bx} dx = A \quad (7)$$

therefore,

$$B_o = B_h(1 - e^{-br}). \quad (8)$$

Following Koschmieder's definition of contrast,

$$\epsilon = \frac{B_h - B_o}{B_h} \quad (9)$$

$$\epsilon = \frac{B_h - B_h(1 - e^{-br})}{B_h} = e^{-br}. \quad (10)$$

Now if  $r$  is defined as the visual range and denoted by  $V_m$ ,

$$V_m = \frac{1}{b} \ln \frac{1}{\epsilon}. \quad (11)$$

Equation (11) is to be used in determining the visual range with natural daylight.

Another set of assumptions will be required for calculation of visual range when artificial lighting prevails. The Allard assumption is that the threshold of vision for a point source of light is a special case of the threshold of brightness contrast. It is more convenient to adopt as a parameter the illuminance produced at the eye by the point source. In derivation of an equation for this assumption, the total visual flux  $F_o$  emitted by a point source is attenuated by absorption and scattering. This effect can be represented by the following equation:

$$dF = \left[ \left( \frac{\partial F}{\partial x} \right)_s + \left( \frac{\partial F}{\partial x} \right)_a \right] dx \quad (12)$$

$$\left( \frac{\partial F}{\partial x} \right)_s = -bF \quad \text{Scattering} \quad (13)$$

$$\left( \frac{\partial F}{\partial x} \right)_a = -kF \quad \text{Absorption} \quad (14)$$

the attenuation coefficient  $\sigma$  is given by

$$b + k = \sigma, \quad (15)$$

and the definition for illuminance  $E$  by

$$E = \frac{dF}{dx} = -\sigma F. \quad (16)$$

By integrating equation (17) between the limits 0 and  $r$ , we get

$$F = F_0 e^{-\sigma r}. \quad (17)$$

Multiplying both sides of the equation by  $(-\sigma)$ , we get

$$-\sigma F = -\sigma F_0 e^{-\sigma r} \quad \text{and} \quad (18)$$

$$E = E_0 e^{-\sigma r}. \quad (19)$$

If the light source is not a collimated beam, the intensity  $I_0$  is reduced further inversely as the square of distance  $r$ , and

$$E_t = \frac{I_0 e^{-\sigma r}}{r^2} \quad (20)$$

where  $E_t$  is defined as the threshold value of  $E$ , or the minimum illuminance needed by the observer to produce the sensation of seeing.

Equation (20) is known as Allard's law when the visual range  $V_m$  is substituted for  $r$ .



$$E_t = \frac{I_o e^{-\sigma V_m}}{V_m^2} \quad (21)$$

Equation (21) can be made more applicable by introduction of the transmissometer reading  $T = e^{-\sigma R}$

$$T^{V_m/R} = e^{-\sigma V_m} \quad (22)$$

Where R is the base line of the transmissometer, in our case 750 ft, equation (21) becomes

$$E_t = \frac{I_o T^{V_m/R}}{V_m^2} \quad (23)$$

Solving for  $V_m$ , equation (24) is obtained.

$$2 \ln V_m + \ln E_t = \ln I_o + \frac{V_m}{R} \ln T \quad (24)$$

The solution of equation (24) can be obtained by the use of Figures 2 and 3, a nomogram with the attenuation coefficient  $\sigma$  as ordinate and the visual range  $V_m$  as the abscissa.

A much more sophisticated solution can be obtained by programming equation (24) for introduction into a digital computer and feeding the transmissometer data directly into the computer. This process would allow it to be incorporated directly into the 433L System.

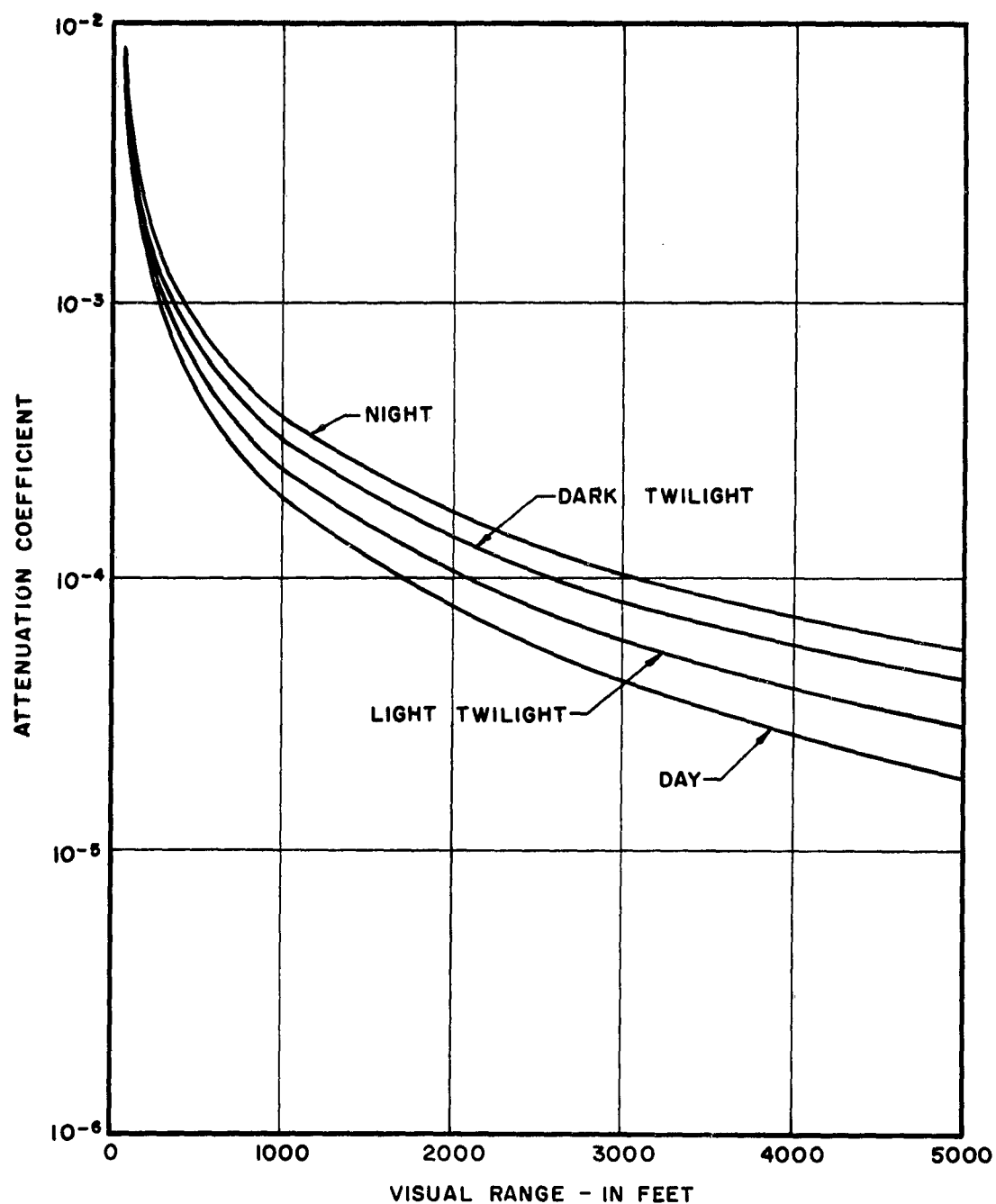


FIG. 2. THE MINIMUM DISTANCE AS A FUNCTION OF THE ATTENUATION COEFFICIENT AS SEEN BY 20 % OF THE PILOTS TESTED BY HAIG AND MORTON.

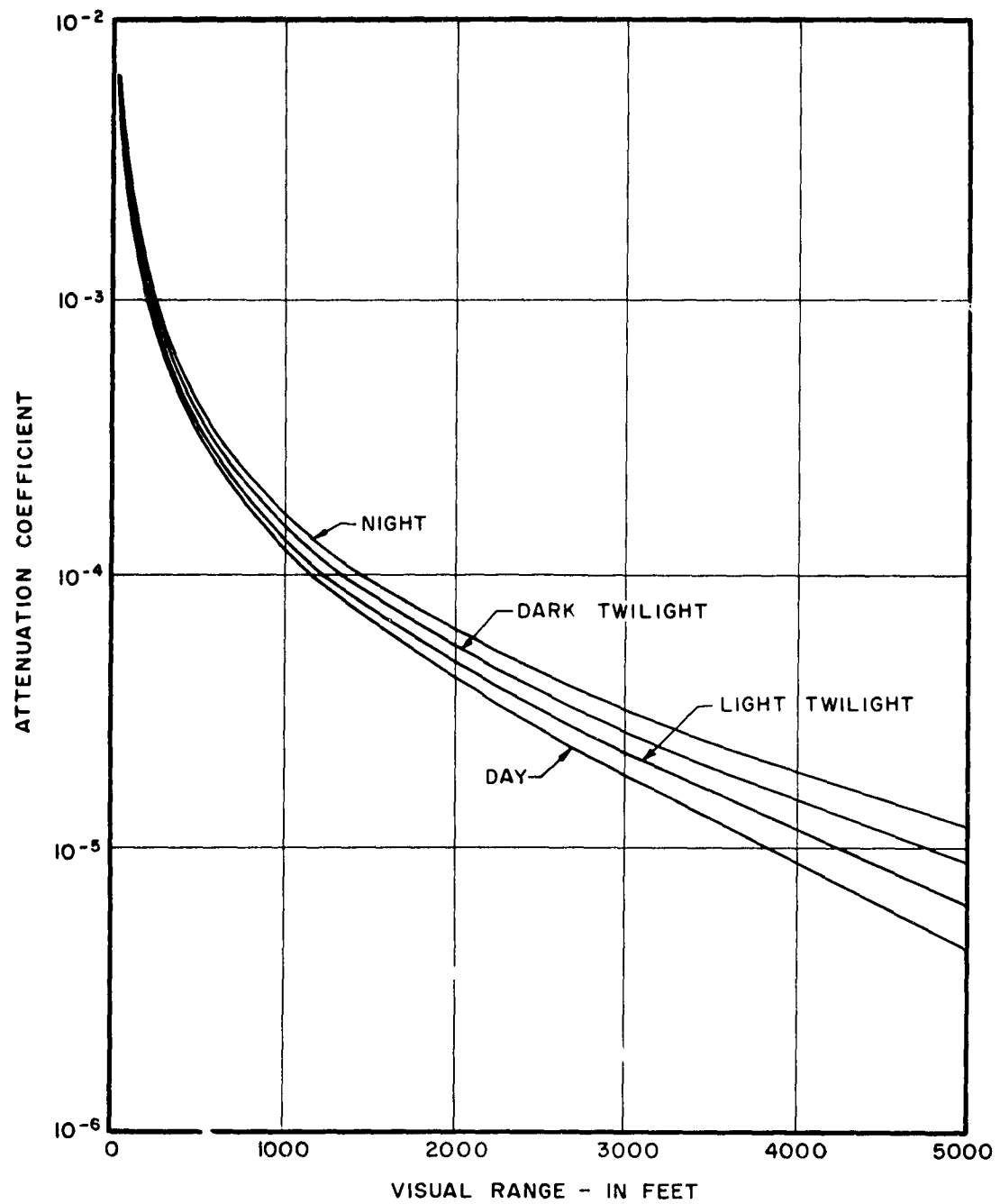


FIG. 3. THE MINIMUM DISTANCE AS A FUNCTION OF THE ATTENUATION COEFFICIENT AS SEEN BY 90% OF THE PILOTS TESTED BY HAIG AND MORTON.

### 3. THRESHOLD OF ILLUMINATION

Equation (24) can be used to determine the visual range when the threshold of illumination from a point source  $E_t$  is known. Haig and Morton (1958) determined what the values of  $E_t$  should be for pilots when various types of background lighting conditions prevailed. The Haig and Morton paper established the threshold of illumination at two levels, based on the individual values of  $E_t$  found for participating pilots. Level 1 was the threshold of illumination at which only 20% of all pilots tested could detect the field landing lights. Level 2 was the threshold of illumination at which 90% of all who participated in the study could detect the same lights.

The threshold of illumination was found to vary with different types of background lighting conditions. Haig and Morton differentiate the background lighting into four classes, i.e., night, dark twilight, bright twilight, and day.

TABLE 1. Threshold of illumination values ( $E_t$ ) (after Haig and Morton).

Background Illuminance Values	$E_t$ lumen/ft <sup>2</sup>	
	20 Percent	90 Percent
Less than 2 lumen/ft <sup>2</sup> (night)	$8.5 \times 10^{-8}$	$6.3 \times 10^{-5}$
2 to 100 lumen/ft <sup>2</sup> (dark twilight)	$6.0 \times 10^{-7}$	$1.0 \times 10^{-4}$
100 to 1200 lumen/ft <sup>2</sup> (bright twilight)	$4.8 \times 10^{-6}$	$1.5 \times 10^{-4}$
1200 lumen/ft <sup>2</sup> or greater (day)	$2.4 \times 10^{-5}$	$2.1 \times 10^{-4}$

The other data needed to solve equation (24) are the length of the base line of the transmissometer and the light intensity of the transmissometer. For standard installations, these are:

$$R = 750 \text{ ft}$$

$$E_o = 10,000 \text{ lumen/ft}^2.$$

At the Newark Airport installation used by Haig and Morton, the values were  $R = 810 \text{ ft}$ , and  $E_o = 10,000 \text{ candlepower}$ . Corrections for these differences have been included in our work in order to make the nomograms applicable to standard installations.

#### 4. EXTINCTION COEFFICIENTS

In order to determine the attenuation of vision by fog and low clouds, the water droplets in suspension are all assumed to be spherical and non-absorbing in the visible region of the spectrum. For the extinction coefficient, van de Hulst (1957) gives equation (25):

$$\sigma = \pi n a^2 Q, \quad (25)$$

where  $n$  is the number of drops per unit volume,  $a$  is drop radius, and  $Q$  is defined as the efficiency factor determined by

$$Q = 2 - \frac{4}{\rho} \sin \rho + \left( \frac{2}{\rho} \right)^2 (1 - \cos \rho). \quad (26)$$

According to van de Hulst, this is one of the most useful formulae in the whole domain of the Mie theory because it describes the salient features of the extinction curve for values of index of refraction between 1 and 2. Index of refraction,  $m$ , is 4/3 for water droplets. van de Hulst defines  $\rho$  by

$$\rho = 2x (m - 1) \quad (27)$$

and  $x$  as

$$x = \frac{2 \pi a}{\lambda} \quad (28)$$

where  $\lambda$  is the predominant wave length in the visible region of the spectrum. For simplification  $\lambda$  was assumed to be equal to  $0.5\mu$ .

Equation (25) provides a method by which the extinction

coefficients of the visual spectrum can be computed if the radius and drop concentration are known. Bricard (1943) and Diem (1942, 1948) published information concerning these parameters of stratus clouds. Bricard gave the mean radius and drop concentration, but Diem gave three characteristic drop radii and concentrations. The characteristic drop radii of Diem are defined as

$r_m$  - the mean radius,

$r_d$  - the mode radius,

$r_p$  - the predominant radius.

The extinction coefficients were computed for the Bricard mean drop radius and each of the Diem characteristic drop radii. For ease in compiling the following case numbers were used:

Case

1. Bricard	$r_m$	mean drop radius
2. Diem	$r_m$	mean drop radius
3. Diem	$r_d$	mode drop radius
4. Diem	$r_p$	predominant drop radius

Table 2 gives the needed information concerning cloud drop distributions and extinction coefficients for each of the above cases.

TABLE 2. Cloud drop size distribution, van de Hulst efficiency factor and attenuation coefficient.

<u>Case</u>	<u>n</u>	<u>r</u>	<u>Q</u>	<u><math>\sigma</math></u>
1.	664 $\frac{\text{drops}}{\text{cm}^3}$	$5.3 \times 10^{-4} \text{ cm}$	1.91977	$11.22 \times 10^{-4} \text{ cm}^{-1}$
2.	260 $\frac{\text{drops}}{\text{cm}^3}$	$6 \times 10^{-4} \text{ cm}$	1.92269	$5.65 \times 10^{-4} \text{ cm}^{-1}$
3.	260 $\frac{\text{drops}}{\text{cm}^3}$	$4 \times 10^{-4} \text{ cm}$	2.10139	$2.75 \times 10^{-4} \text{ cm}^{-1}$
4.	260 $\frac{\text{drops}}{\text{cm}^3}$	$9 \times 10^{-4} \text{ cm}$	2.03397	$13.46 \times 10^{-4} \text{ cm}^{-1}$



## 5. COMPUTATION OF VISUAL RANGE

The following visual ranges were determined for each of the attenuation coefficients of Table 2. The visual ranges were computed for each of the threshold of illumination values ( $E_t$ ) described by Haig and Morton (1958). These data are given in Tables 3-5 inclusive.

TABLE 3. The minimum distance that 20% of pilots tested by Haig and Morton could see.

<u>Case</u>	<u>day</u>	<u>bright twilight</u>	<u>dark twilight</u>	<u>night</u>
1	260 ft	298 ft	353 ft	397 ft
2	445 ft	524 ft	616 ft	717 ft
3	778 ft	930 ft	1125 ft	1329 ft
4	222 ft	260 ft	296 ft	345 ft

TABLE 4. The minimum distance that 90% of pilots tested by Haig and Morton could see.

<u>Case</u>	<u>day</u>	<u>bright twilight</u>	<u>dark twilight</u>	<u>night</u>
1	204 ft	210 ft	218 ft	224 ft
2	350 ft	362 ft	380 ft	400 ft
3	586 ft	615 ft	649 ft	692 ft
4	182 ft	186 ft	194 ft	202 ft

TABLE 5. The visual ranges for conditions of natural light obtained by use of the Koschmieder equation (12).

<u>Case</u>	<u>V<sub>m</sub></u>
1	114 ft
2	226 ft
3	465 ft
4	95 ft

The comparison between visual ranges of natural light and the visual ranges determined through use of Allard's law with the described lights for daylight conditions are given in Table 6.

TABLE 6. Visual ranges for daylight conditions, comparing Koschmieder and Allard methods.

<u>Case</u>	<u>V<sub>m</sub> - nat.</u>	<u>V<sub>m</sub> - 20</u>	<u>V<sub>m</sub> - 90</u>
1	114 ft	260 ft	204 ft
2	226 ft	445 ft	350 ft
3	465 ft	778 ft	586 ft
4	95 ft	222 ft	182 ft

The results obtained from these formulae appear to give a very good first order approximation of the visual range in clouds and fog. From these results, an approximate method for determining the mass of water suspended in a cloud or fog formation can be developed.

The mass of cloud water per unit volume is

$$w = \frac{4}{3} \frac{\bar{a} \sigma \delta}{Q} \quad (29)$$

where  $\delta$  is the density of water.

In application of this equation, the water density in the four cases examined would be shown in Table 7.

TABLE 7. Water density for the four types of clouds studied.

<u>Case</u>		
1	$4.12 \times 10^{-7} \text{ gm/cm}^3$	or $0.412 \text{ gm/m}^3$
2	$23.50 \times 10^{-8} \text{ gm/m}^3$	$0.235 \text{ gm/m}^3$
3	$6.98 \times 10^{-8} \text{ gm/cm}^3$	$0.0698 \text{ gm/m}^3$
4	$7.96 \times 10^{-7} \text{ gm/cm}^3$	$0.796 \text{ gm/cm}^3$

It should be noted that Diem (1942, 1948) gives several characteristic drop parameters, and each of these parameters gives a different density of liquid water in the cloud and different

visual range. This variation emphasizes that an approximation is the best which can be hoped for until new measurements become available.

There is an interesting relationship between visual range, the size of the droplets, and the water content of fogs. This relationship is even more striking when Findeisen's paper (1932) is considered. He found evidence for the coalescence of droplets in an artificial fog and stated that aging of fog is associated with a shift in drop size spectrum to larger sizes.

If this theory is correct, visual range should increase as fog ages. In order to examine the effect of the Findeisen theory, we have calculated visual range for four new cases. Each is a fog having the same liquid water content as one of those listed in Table 2, but with drop radius twice that listed in Table 2. Visual ranges calculated for the two sets of drop size distribution are given in Table 8, which shows, of course, that visual ranges are greater in fogs with the larger (and fewer) drops.

TABLE 8. The variation of visual range in an aging fog.

Case	Day		Bright Twilight		Dark Twilight		Night (1)	
	New Fog	Aged Fog	New Fog	Aged Fog	New Fog	Aged Fog	New Fog	Aged Fog
1-20	260	435	298	510	353	600	397	695
1-90	204	340	210	355	218	370	224	390
2-20	445	740	524	890	616	1070	717	1260
2-90	350	560	362	590	380	620	400	660
3-20	778	1360	930	1670	1125	2060	1329	2460
3-90	586	970	615	1030	649	1095	692	1175
4-20	222	390	260	460	296	540	345	625
4-90	182	310	186	325	194	340	202	355

(1) All visual ranges are given in feet.

## 6. CONCLUSION

This investigation indicated the feasibility of using a method such as has been described here in an automatic weather observing and forecasting system such as the 433L System.

The Findeisen claim that the coalescence of droplets in an artificial fog shifts the drop size spectrum to larger sizes and the Langmuir theory which says that the smaller droplets would tend to evaporate give strong support to the idea that visual ranges should increase as a fog ages.

## REFERENCES

- Allard, E., 1876: Mémoire sur l'intensité et la Portée des phares, Dunod, Paris.
- Bricard, S., 1943: La Teneur des Nauages en Eau Condensée, La Meteorologie, p. 57.
- Diem, M., 1942: Messungen der Grösse von Wolkenelementen I, Ann der Hydrogr. 70, p. 142.
- Diem M., 1948: Messungen der Grösse von Wolkenelementen II, Met. Rundschau 1, p. 261.
- Findeisen, W., 1932: Messungen der Grösse und Anzahl der Nebeltropfen zum Studium der Koagulation inhomogenen Nebels, Beitr. Geophy. 35, p. 295.
- Haig, T. O., and W. O. Morton, 1958: An Operational System to Measure, Compute, and Present Approach Information, Air Force Surveys in Geophysics, No. 202. Project 7694. Air Force Cambridge Research Laboratories, Bedford, Massachusetts.
- van de Hulst, H. W., 1957: Light Scattering by Small Particles, John Wiley & Sons, Inc., New York.
- Johnson, S. C., 1954: Physical Meteorology, John Wiley and Sons, Inc., New York.
- Koschmieder, H., 1924: Theorie der horizontalen Sichtweite, Beitr. Phys. Freien Atm., 12: 33-53; 171-181.
- Langmuir, I., 1944: Supercooled Water Droplets in Rising Currents of Cold Saturated Air, G. E. Research Laboratory, Report W-33-106-SC-65.
- Mason, B. J., 1957: The Physics of Clouds, Clarendon Press, Oxford.
- Middleton, W. E. L., 1952: Vision Through the Atmosphere, University of Toronto Press, Toronto.